# **CONTROL SYSTEM FOR HOT WIRE ANEMOMETRY**





### **DESIGN REQUIREMENTS**

Air flows at 10 - 15 m/s can contain velocity fluctuations up to 15 kHz. In hot wire anemometry, a thin wire (5  $\mu m$ thick and 2 mm long, usually platinum) is submerged in a flow and comprises a leg of Wheatstone bridge (Rw). Current is supplied to the microscale wire through the Wheatstone bridge. While this current produces Joule heating in the wire, fluid flowing over it convects the heat away causing Rw to change. Therefore, by using principles of heat transfer and electronics,  $V_0$  measured can be correlated with flow velocity to extract high frequency content. However, the ability to measure high frequencies is dependent on the properties of the wire and electrical system, which must be characterized.

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### **DESIGN ALTERNATIVES**

The design alternatives considered in this project are Constant Current Anemometer (CCA), Constant Voltage Anemometer (CVA), and Constant Temperature Anemometer (CTA). The CCA circuit does not provide high enough temporal resolution to extract high frequency content from the velocity fluctuations. The CTA and CVA employ feedback mechanisms to improve the temporal resolution. CTA is significantly more complex than the CCA and is not feasible to analyze in the constrained time. Therefore, the below sections fully characterize CCA, CVA, and outline the satisfactory results of the CVA model.

The circuit diagram alongside is the CCA circuitry. Resistors Rx's are in 10's of kiloohms to ensure constant current through Rw (wire) is constant. As Rw changes due to heat convection in fluid flow, voltage across the  $\frac{\Delta R_w}{\Delta u}(s) = -\frac{K}{\tau_w s + \tau_w s$ 

 $\tau_w s + 1$ 

**Constant Current Anemometer (CCA)** bridge is captured via an Instrumentation amplifier. The differential equation governing the dynamics of the hot wire and the circuitry is used to obtain the transfer function (TF) ( $\Delta R_w/\Delta u$ ) of the CCA model; the TF is a relationship of the change in wire resistance for a step change in fluid velocity. The TF helps in determining the step response of the CCA or CVA system which elucidates the frequencies the system can resolve. The parameter K is governed by the gain of the op-amp, ratio of Wheatstone bridge resistors, and fluid properties of air while  $\tau_w$  is determined by the thermal properties of the wire. *s* is Laplace the variable.



Above are the step responses of CCA's (left) and CVA's (right) step response. The 95% criteria (system reaches 95% of steady state response in three time constants of time) is used to extract time constants of the systems. The time constant,  $\tau_{CCA}$  of CCA is 0.567 ms. This corresponds to a -3dB frequency of 280 Hzn(-3dB) frequency is the frequency at which the system produces a signal attenuation of -3dB). However, the velocity fluctuation the needed to be resolved are upto 15 kHz. The CVA has a settling time,  $\tau_{s.5\%} = 15.3 \mu s$ . This corresponds to -3dB frequency of 10.4 kHz, which is a significant improvement from the CCA. The feedback resistors and capacitors (Ra, Rb, Rd and C) can be tuned to introduce a zero at the location of the wire's pole iso that the dynamics are dominated by op-amp's and Rd's feedback response, encapsulated by B and Tc, which are again determined during the fine-tuning process. The top right figures show experimental results of the CCA and CVA circuits. The CCA graph (left) follows the King's law (a power law relationship) between the measured voltage and flow speed. Similarly, the CVA also follows a power law relationship between the measured voltage and wire resistance. These are the calibration curves that can now be used to estimate wind speed after measuring voltages over some time.



design alternatives identified – constant current (CCA), constant temperature (CTA), and constant voltage (CVA). For CCA, thermal balance equation guided the analysis in obtaining the transfer function and step response. The wire's first order system combined with the CVA's op-amp response resulted in a higher order transfer function. This transfer function was compensated and finally tuned to give the desired response. The developed circuit was tested in the wind tunnel as shown in Fig. 3.

### **DISCUSSION, CONCLUSION &** RECOMMENDATIONS

**Discussion and Conclusion.** This project designed, analyzed, and tested two modes of hot wire anemometry, CCA and CVA. The response of CCA has a -3dB frequency of 280 Hz, which is cancelled with a zero in the compensated circuit of the CVA (-3dB @ 10.4 kHz). This results in a much faster response in CVA, one that can be tuned as per the needs of a research lab. This project provides a robust and inexpensive means of hot wire anemometry to small research laboratories that may not be able to afford industrial anemometers **Recommendations.** In the future CCA and CVA's step response could be captured in a Wind Tunnel. In addition, the Constant Temperature Anemometer should be characterized. Finally, the advantages and disadvantages of CCA, CVA, and CTA should be cataloged systematically.

Resources.







Fig. 2. Top and bottom show figures CCA and CVA operation respectively. Both are callibration curves that can be used to estimate wind speed or wire resistance from voltage measurements.

### **DESIGN EVALUATION & ITERATIVE PROCESS**



Fig. 3. Hot wire in a wind collecting data. experimental Research was done to understand each of the

### REFERENCES

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